

# Reliability Validation of Components (1)

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# Introduction

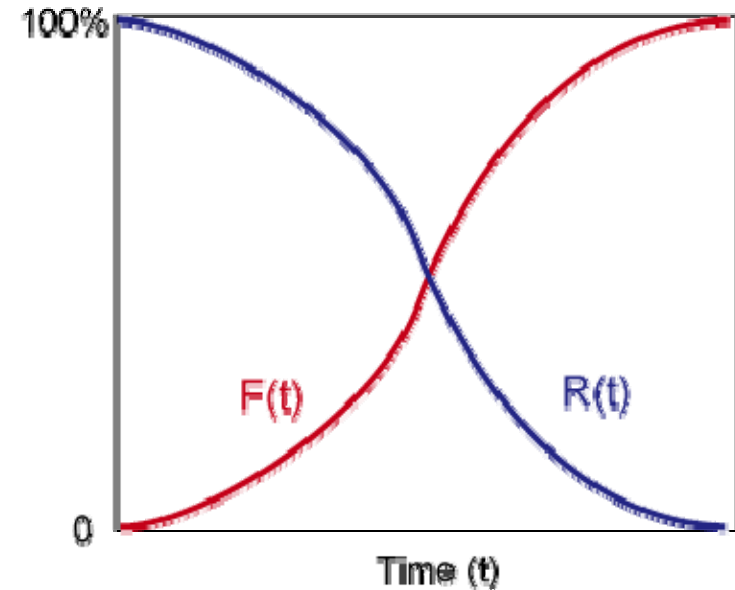
- First: Summary of the terminology and the types of failure profiles to consider.
- Second: Attempt at analyzing the level of reliability validation which might be possible at a test ML for ILC.
- Warning and disclaimer: I started serious reading of textbooks only last week → I can be VERY wrong.

# References

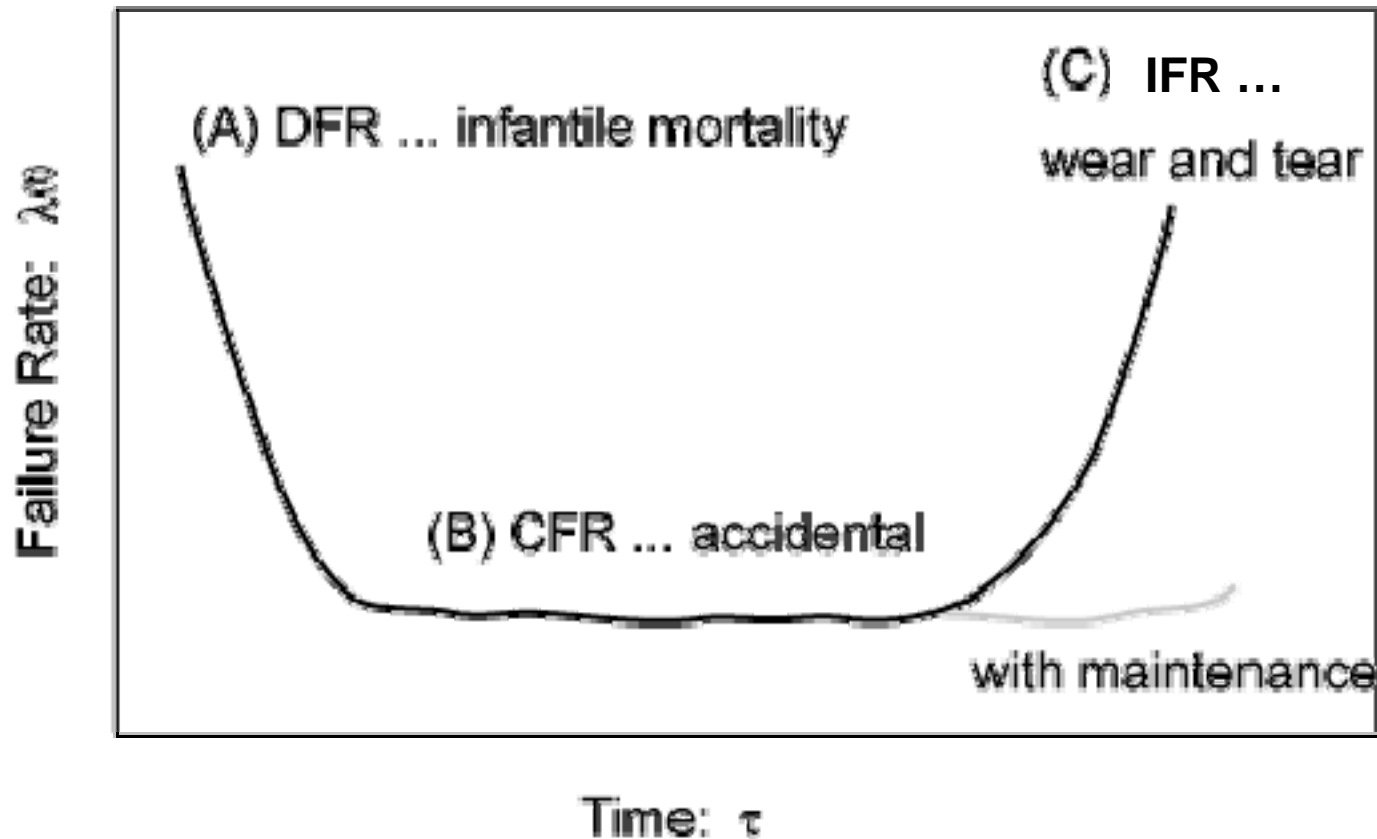
- Introduction to Reliability Engineering (信頼性工学入門 )  
H.Shiommi (塩見 弘) , Rev. 3, 2001, Maruzen (丸善 )
- Reliability Engineering Series (日科技連信頼性工学シリーズ ) 1984, Union of Japanese Scientists and Engineers (日科技連)
- Practical Reliability Engineering, P.O'Conner, 2002, John Willey and Sons. [Still waiting for delivery from Amazon]

# Terminology

- Reliability Function:  $R(t) =$  probability (or fraction) of items running without failure as function of time.
- Failure Distribution Function:  $F(t) =$  probability of item failure as function of time. Note:  $R(t) = 1 - F(t)$
- Failure Rate Function:  $\lambda(t) =$  rate at which the items, who survived the preceding operation time of  $t$ , would fail:  $\lambda(t) = -(\frac{d R(t)}{dt}) / R(t)$  , hence  $R(t) = \exp[-\int \lambda(s) ds]$
- $MTBF = \int R(t) dt$ , where the integral is over  $0 \rightarrow \infty$



# Typical Time Profile of Item Failures (1)



# Typical Time Profile of Item Failures (2)

- DFR (Decreasing failure rate distribution)
  - The  $\lambda(t)$  is non-increasing func of  $t$ .
  - E.g. “initial” state (infantile mortality) where good and bad lots are mixed.
  - $R(t) = p \exp(-\lambda_1 t) + (1-p) \exp(-\lambda_2 t)$  , with  $\lambda_1 \gg \lambda_2$
- CFR (Constant failure rate distribution)
  - The  $\lambda(t)$  is ~constant.
  - E.g. “matured state” case where failures are random and accidental
  - $R(t) = \exp(-\lambda t) = \exp(-t/MTBF)$ ;  $\lambda = 1/MTBF$
- IFR (Increasing failure rate distribution)
  - When  $\lambda(t)$  is an increasing func of  $t$ .
  - Life limit due to wear and tear

# Evaluation of MTBF (1)

- If a sufficient number ( $r > 15$ ) of failures could be observed, an analysis which assumes a Gaussian distribution of TBF is likely to be adequate. i.e.,
- One can execute a standard “mean and sigma” analysis of failure times of the samples and compute the MTBF or estimate its upper/lower limits at adequate confidence levels.

# Evaluation of MTBF (2)

- If only less than several instances of failure samples are available, the analysis may have to depend on the underlying model of  $\lambda(t)$ , which could be also unknown (catch-twenty-two situation).
  - Rescue formula: In case  $\lambda(t)$  is assumed constant (CFR)
    - $T$  = total operation time
    - $r$  = # of failures observed in  $T$
    - Then,  $2r \text{ MTBF} / \langle \text{MTBF} \rangle$  will obey a  $\chi^2$  distribution with  $\text{DOF} = 2r$



# Evaluation of MTBF (3)

- If no failures are observed during the total operation time of  $T$  (either because  $T$  being too short or MTBF being too long), one can only estimate the limit value of MTBF or others. A couple approaches are possible:
  - Calculate the limit of reliability (which is usually not too useful anyways), or
  - Calculate the reliability and MTBF with a “worst case” assuming  $r = 1$ .
  - Calculate the limit of  $\lambda$  while assuming an exponential failure rate function.

# Very Simple Case Study (1)

- 24 cryomodules (or whatever), each running over 1000 hrs, gave zero failure. What does this mean?
- This means zero failure in 24,000 total operation hours. OK. Still, what does this mean?
- Three types of analyses as per the previous page (only the results are shown. Consult textbooks for derivations):
  - Assuming Poisson distribution for # of failures ( $r$ ), the lower limit (90% CL) of reliability over 24,000 hrs operation is  $\sim 0.9$ .
  - By taking the number of failure  $r = 1$  as the most pessimistic scenario, we calculate the upper and lower limits (90% CL) of MTBF as:
    - $MTBF_U = 24 \times 1000 \times 19.4 = 4.6 \times 10^5$  hrs, and
    - $MTBF_L = 24 \times 1000 \times 0.21 = 5040$  hrs
  - Assuming exponential distribution for the failure rate function with constant  $\lambda$ , the 90% CL of  $\lambda$  is given as  $\lambda_u = 2.3/T_{total}$ . Hence,
    - the  $\lambda_u = 2.3/(1000 \times 24) = 9.58 \times 10^{-5}$ .
    - $MTBF_L = 1/\lambda_u = 10,000$  hrs

# Very Simple Case Study (2)

- We want to establish  $MTBF > 10^5$  hrs with 90% CL for a kind of component. What should we do?
- We take the constant  $\lambda$  model. In case we try to evaluate  $MTBF_L$  with  $T_{tot}$  hours of total operation time, in which zero failure is found:
  - $MTBF_L = 1/\lambda_u = T_{tot}/2.3$
  - $\rightarrow T_{tot} = 2.3 \times MTBF_L = 230,000$  hrs is required.
- We need to observe zero failure with:
  - 192 units running in parallel for 1,200 hrs ( 50 days)
  - 24 units ... for 9,600 hrs ( 400 days)
  - 8 units ... for 28,800 hrs (1200 days)

# Observations and Remarks for Further Study (1)

- Proper use of standard terminology is important. It is for discussing the reliability issues among parties with varying background and expertise. We should learn IEC 60050 (JIS Z 8115:2000) as the common language. Some teach-in might be worth, not only for S2/RDB but eventually for the entire GDE.
- Before discussing the issues with MTBF in the “constant failure” regime with confidence, we naturally have to address the issues with : “line debugging”, “infantile mortality” and “initial burn-in”. We have to develop ways to separate these from the “constant failure rate” regime?
- A cursory look indicates that it will not be too easy to establish  $MTBF > 10^5$  hrs with the level of test period and the number of units that are easily conceivable in pre-construction testing for ILC. Most likely these tests will only tell us if our production lines “are (or are not) contaminated by major bugs.”

# Observations and Remarks for Further Study

(Continued) Therefore,

- Techniques of “accelerated testing” and “component-level mass testing” would be useful, but perhaps they are not applicable to all critical components.
- Techniques of FTA (Failure Tree Analysis) need to be looked into, also, and should be put into the perspective.
- Such efforts might go well beyond the original scope of S2, and could well be spelled out as the issue to address by GDE Engineering in the next N years.
- All I said here could be substantially wrong (since I am learning only recently). → Colleagues, please, cross-examine and check!